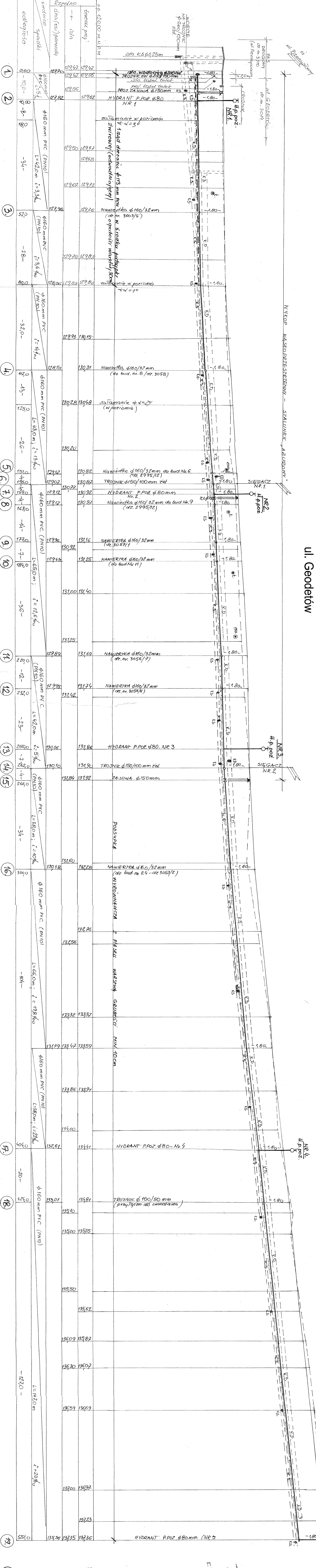


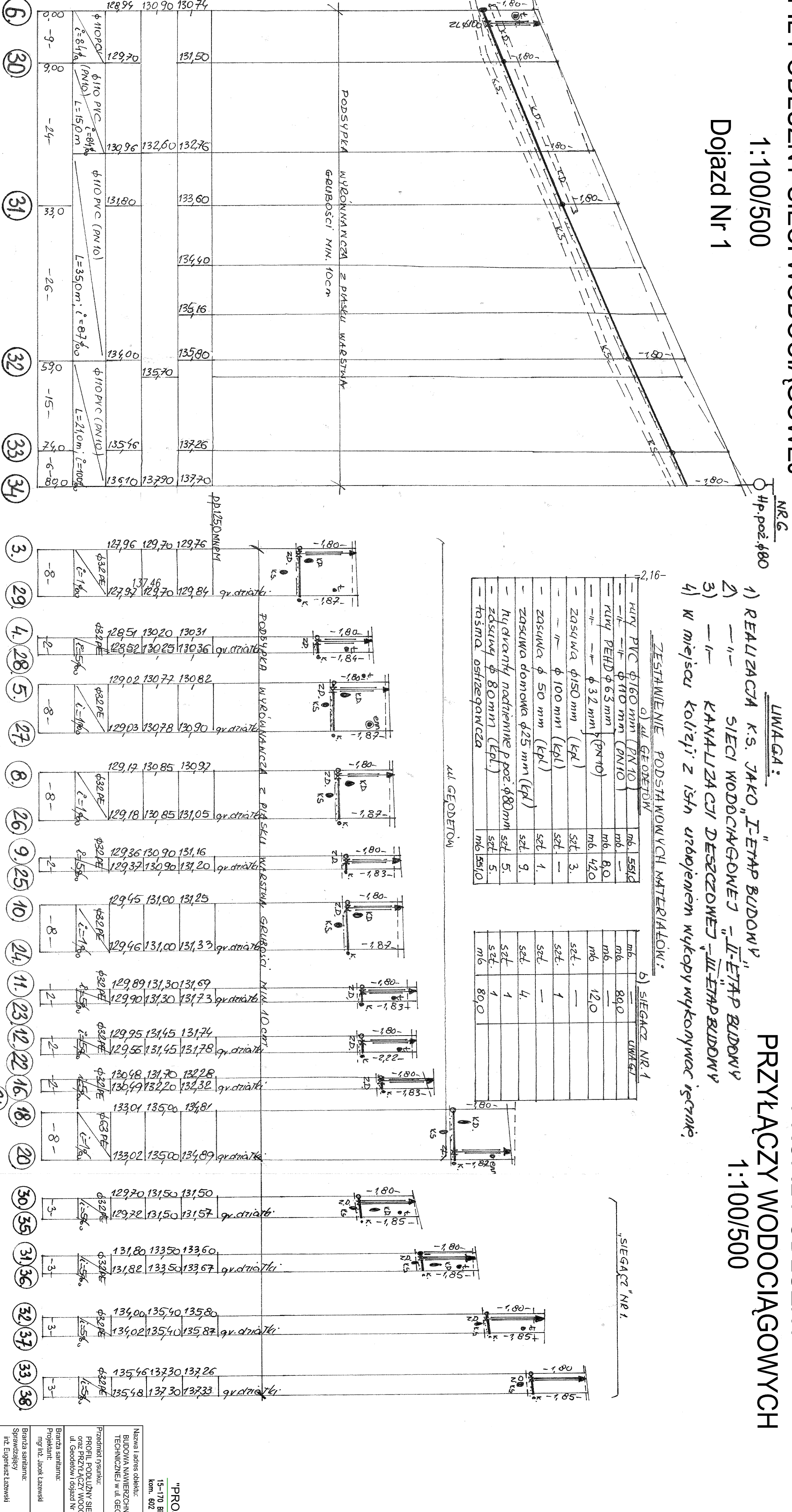
1:100/500

ul. Geodetów



1:100/500

Dojazd Nr 1



1) REALIZACJA K.S. JAKO „I-ETAP BUDOWY”
2) — „—”
3) SIECI WODOCIECIAGOWEJ — „II-ETAP BUDOWY”
4) KANALIZACJI DESZCZOWEJ — „III-ETAP BUDOWY”
W miejscu kolidują z sobą urzędowym wykopy wykonawców i instalacje

1:100/500

| | | | |
|---------------------------------------|-------------------------|---------|-----|
| — ruy pvc | φ 60 mm (PVC) | m.b. | 89. |
| — — | φ 70 mm (PVC) | m.b. | 89. |
| — ruy PEAD | φ 65 mm (PEAD) | m.b. | 89. |
| — — | φ 32 mm (PEAD) | m.b. | 12. |
| — ZASLAVA | φ 50 mm (EPL) | szt. 3. | — |
| — — | φ 100 mm (EPL) | szt. 1 | — |
| — ZASLAVA | φ 50 mm (EPL) | szt. 4. | — |
| — ZASLAVA | nadmienne φ 25 mm (EPL) | szt. 9. | — |
| — hydrauliczne nadmienne poz. φ 80 mm | | szt. 5. | — |
| — zasilanie φ 80 mm (EPL) | | szt. 5. | — |
| — tożyma osłazewaczka | | m.b. | 89. |

Diagram of a beam with a point load P at distance x from the left support and a uniformly distributed load q over a length l . The beam is supported by a pin at the left end and a roller at the right end. The total length of the beam is 1.50 m . The point load P is 5 kN . The uniformly distributed load q is 1 kN/m . The distance x is 0.5 m . The reaction at the left support is 5 kN . The reaction at the right support is 10 kN . The maximum deflection is 0.01 m .

16-
ZESTAWIENIE PODSTAWOWYCH MATERIAŁÓW:

[illegible]

| | | | |
|---|-----------------------|---------|---|
| — | rwv PEHD $\phi 63$ mm | | |
| | (PN 10) | mb. 8.0 | |
| | | mb | — |

[illegible]

| | | |
|------------------------|---------|--------|
| - ZAS4WA $\phi 150$ mm | Set. 3. | Set. — |
|------------------------|---------|--------|

| | | | |
|---|-----------------------------|------|---|
| - | $\phi 100 \text{ mm}$ (Köl) | Szt. | - |
| - | " " | Szt. | 7 |

| | | | |
|---|--------------|--------|---|
| — | 245 mm (KPC) | sec 1. | — |
| — | 245 mm (KPC) | sec 1. | — |

| | | |
|---|------|----|
| 2135LWA 08110WA ϕ 2.5 mm (Lp) | SEC. | 3. |
| 4. d. 0.001 perforations a row of 80 mm | SEC. | 4. |

| | | | |
|-----------------------|-----|-----|---|
| - 300mm x 80mm (EOL) | 5.0 | 5.0 | 1 |
| - 100mm x 100mm (EOL) | 5.0 | 5.0 | 1 |
| - 100mm x 100mm (EOL) | 5.0 | 5.0 | 1 |

| | | |
|-----------------------|----|------|
| - tashma oshizgan/cza | m6 | 55,0 |
|-----------------------|----|------|

| | |
|----|------|
| m6 | 80,5 |
|----|------|

100

AL. GEODETOM

[illegible]

87-
80-
87
80
18
180
8
-18
-1
5

[illegible]

Handwritten musical notation on a staff. It includes a treble clef, several notes (some with stems), and rests. There are also some markings that look like '37' and '1, 1, 1' above the staff.

2D. KS

22.

5. PODBYPKA WYRÓWNAJĄCA Z PIASKU WARSTW GRUBOŚCI MIN.

strate
strate
strate
strate
strate
strate

[illegible]

| | |
|---|---|
| 4 | 9 |
| 5 | 9 |
| 2 | 9 |
| 2 | 9 |
| 2 | 9 |
| 5 | 9 |
| 0 | 9 |
| 3 | 9 |
| 9 | 9 |
| 3 | 9 |

9,8
30,3
30,3
30,8
30,9
30,9
31,0
31,16
31,2
31,25
31,3
31,6
31,7

| | |
|---|----|
| 0 | 12 |
| 0 | 13 |
| 5 | 13 |
| 2 | 13 |
| 8 | 13 |
| 5 | 13 |
| 5 | 13 |
| 0 | 13 |
| 0 | 13 |
| 0 | 13 |
| 0 | 13 |
| 6 | 07 |
| 0 | 74 |

$\frac{46}{9,70}$
 $\frac{0,20}{0,23}$
 $\frac{0,7}{0,78}$
 $\frac{0,85}{0,88}$
 $\frac{0,9}{0,99}$
 $\frac{31,0}{31,3}$
 $\frac{31,3}{31,36}$

| | | |
|-----|----|----|
| 137 | 2 | 12 |
| 1 | 13 | |
| 2 | 13 | |
| 2 | 13 | |
| 3 | 13 | |
| 2 | 13 | |
| 8 | 13 | |
| 6 | 13 | |
| 7 | 1 | |
| 5 | 1 | |
| 6 | 1 | |
| 89 | 1 | |
| 20 | 1 | |

27,94
28,5
28,5
29,0
29,0
29,1
29,1
29,3
29,3
29,4
29,4
29,5
29,5

[illegible]

$\frac{1}{2} = 0.5$
 $\frac{1}{3} = 0.333$
 $\frac{1}{4} = 0.25$
 $\frac{1}{5} = 0.2$
 $\frac{1}{6} = 0.166$
 $\frac{1}{7} = 0.143$
 $\frac{1}{8} = 0.125$
 $\frac{1}{9} = 0.111$
 $\frac{1}{10} = 0.1$
 $\frac{1}{11} = 0.091$
 $\frac{1}{12} = 0.083$
 $\frac{1}{13} = 0.077$
 $\frac{1}{14} = 0.071$
 $\frac{1}{15} = 0.067$
 $\frac{1}{16} = 0.0625$
 $\frac{1}{17} = 0.059$
 $\frac{1}{18} = 0.056$
 $\frac{1}{19} = 0.053$
 $\frac{1}{20} = 0.05$
 $\frac{1}{21} = 0.048$
 $\frac{1}{22} = 0.045$
 $\frac{1}{23} = 0.043$
 $\frac{1}{24} = 0.042$
 $\frac{1}{25} = 0.04$
 $\frac{1}{26} = 0.038$
 $\frac{1}{27} = 0.037$
 $\frac{1}{28} = 0.036$
 $\frac{1}{29} = 0.034$
 $\frac{1}{30} = 0.033$
 $\frac{1}{31} = 0.032$
 $\frac{1}{32} = 0.031$
 $\frac{1}{33} = 0.030$
 $\frac{1}{34} = 0.029$
 $\frac{1}{35} = 0.029$
 $\frac{1}{36} = 0.028$
 $\frac{1}{37} = 0.027$
 $\frac{1}{38} = 0.026$
 $\frac{1}{39} = 0.026$
 $\frac{1}{40} = 0.025$
 $\frac{1}{41} = 0.024$
 $\frac{1}{42} = 0.024$
 $\frac{1}{43} = 0.023$
 $\frac{1}{44} = 0.023$
 $\frac{1}{45} = 0.022$
 $\frac{1}{46} = 0.022$
 $\frac{1}{47} = 0.021$
 $\frac{1}{48} = 0.021$
 $\frac{1}{49} = 0.020$
 $\frac{1}{50} = 0.02$
 $\frac{1}{51} = 0.0196$
 $\frac{1}{52} = 0.0192$
 $\frac{1}{53} = 0.0189$
 $\frac{1}{54} = 0.0185$
 $\frac{1}{55} = 0.0182$
 $\frac{1}{56} = 0.0179$
 $\frac{1}{57} = 0.0175$
 $\frac{1}{58} = 0.0172$
 $\frac{1}{59} = 0.0170$
 $\frac{1}{60} = 0.0167$
 $\frac{1}{61} = 0.0164$
 $\frac{1}{62} = 0.0161$
 $\frac{1}{63} = 0.0159$
 $\frac{1}{64} = 0.0156$
 $\frac{1}{65} = 0.0154$
 $\frac{1}{66} = 0.0152$
 $\frac{1}{67} = 0.0149$
 $\frac{1}{68} = 0.0147$
 $\frac{1}{69} = 0.0145$
 $\frac{1}{70} = 0.0143$
 $\frac{1}{71} = 0.0141$
 $\frac{1}{72} = 0.0139$
 $\frac{1}{73} = 0.0137$
 $\frac{1}{74} = 0.0135$
 $\frac{1}{75} = 0.0133$
 $\frac{1}{76} = 0.0132$
 $\frac{1}{77} = 0.0130$
 $\frac{1}{78} = 0.0128$
 $\frac{1}{79} = 0.0127$
 $\frac{1}{80} = 0.0125$
 $\frac{1}{81} = 0.0123$
 $\frac{1}{82} = 0.0122$
 $\frac{1}{83} = 0.0120$
 $\frac{1}{84} = 0.0119$
 $\frac{1}{85} = 0.0118$
 $\frac{1}{86} = 0.0116$
 $\frac{1}{87} = 0.0115$
 $\frac{1}{88} = 0.0114$
 $\frac{1}{89} = 0.0112$
 $\frac{1}{90} = 0.0111$
 $\frac{1}{91} = 0.0110$
 $\frac{1}{92} = 0.0109$
 $\frac{1}{93} = 0.0108$
 $\frac{1}{94} = 0.0106$
 $\frac{1}{95} = 0.0105$
 $\frac{1}{96} = 0.0104$
 $\frac{1}{97} = 0.0103$
 $\frac{1}{98} = 0.0102$
 $\frac{1}{99} = 0.0101$
 $\frac{1}{100} = 0.01$

| | | | | |
|-------------------|------------------------|------------------------|------------------------|------------------------|
| $\log_{10} 1 = 0$ | $\log_{10} 2 = 0.3010$ | $\log_{10} 3 = 0.4771$ | $\log_{10} 4 = 0.6021$ | $\log_{10} 5 = 0.6990$ |
|-------------------|------------------------|------------------------|------------------------|------------------------|

$$\begin{array}{c} \frac{1}{00} \\ \frac{1}{1} \end{array} \quad \begin{array}{c} \frac{1}{1} \\ \frac{1}{1} \end{array} \quad \begin{array}{c} \frac{1}{00} \\ \frac{1}{1} \end{array} \quad \begin{array}{c} \frac{1}{2} \\ \frac{1}{1} \end{array} \quad \begin{array}{c} \frac{1}{00} \\ \frac{1}{1} \end{array} \quad \begin{array}{c} \frac{1}{2} \\ \frac{1}{1} \end{array}$$

| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|-----|
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 32 | 33 | 34 | 35 | 36 | 37 | 38 | 39 | 40 | 41 | 42 | 43 | 44 | 45 | 46 | 47 | 48 | 49 | 50 | 51 | 52 | 53 | 54 | 55 | 56 | 57 | 58 | 59 | 60 | 61 | 62 | 63 | 64 | 65 | 66 | 67 | 68 | 69 | 70 | 71 | 72 | 73 | 74 | 75 | 76 | 77 | 78 | 79 | 80 | 81 | 82 | 83 | 84 | 85 | 86 | 87 | 88 | 89 | 90 | 91 | 92 | 93 | 94 | 95 | 96 | 97 | 98 | 99 | 100 |
|---|---|---|---|---|---|---|---|---|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|-----|

29. 4. 28. 5. 27. 8. 26. 9. 25. 10. 24. 11. 23.

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|---|--------------------------------------|
| JEKT™ Jacek Łazewski ul. Armii Ludowej 58 tel.: 005 675 36 11 50-333 email: je@je-kt.pl je-kt.pl | |
| III INFRASTRUKTURA OŚCIEŃ W GOSPODARSTWIE | Wzrost Płeć: m. Wiek: 1;00/000 |
| CI CACONATCH | Data: 28/10/2010 |
| Uzasadnienie: Wzrost jest 100% (100%) powyżej normy, nie ma żadnych objawów choroby, nie ma żadnych objawów choroby, nie ma żadnych objawów choroby. | Płeć: |
| Uzasadnienie: Wzrost jest 100% (100%) powyżej normy, nie ma żadnych objawów choroby, nie ma żadnych objawów choroby, nie ma żadnych objawów choroby. | Płeć: |